

Comparison of different time splitting algorithms for positive definite advection

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advection schemes in the COSMO model

- 1d advection
 - time splitting algorithm required (e.g. Strang splitting)
- flux form advection
 - volume specific quantities needed
 - density advection required
- time splitting errors destroy consistency
 - density advection required

The time splitting problem

for simplicity: upstream advection, Courant number 0.5

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

scalar [*/kg]

1	1	1	1
1	1	1	1
1	1	2	1
1	1	1	1

The time splitting problem

for simplicity: upstream advection, Courant number 0.5

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

Diagram illustrating the density field on a 4x4 grid. Red arrows indicate upstream advection from right to left. The value in the cell (row 3, column 3) is 1, and red arrows point from it to the cells (row 2, column 3), (row 3, column 2), and (row 3, column 1).

scalar [$^{**}/m^3$]

1	1	1	1
1	1	1	1
1	1	2	1
1	1	1	1

Diagram illustrating the scalar field on a 4x4 grid. Red arrows indicate upstream advection from right to left. The value in the cell (row 3, column 3) is 2, and red arrows point from it to the cells (row 2, column 3), (row 3, column 2), and (row 3, column 1).

The time splitting problem

for simplicity: upstream advection, Courant number 0.5

y-x advection

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

Red arrows indicate advection: horizontal arrows from left to right in the third row, and vertical arrows from bottom to top in the third column.

density

		1	
		1	
1	1	1	

scalar [$**/m^3$]

1	1	1	1
1	1	1	1
1	1	2	1
1	1	1	1

Red arrows indicate advection: horizontal arrows from left to right in the third row, and vertical arrows from bottom to top in the third column.

scalar [$**/m^3$]

		1	
		1.5	
1	1	1.5	

The time splitting problem

for simplicity: upstream advection, Courant number 0.5

y-x advection

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

Red arrows indicate advection: horizontal arrows from left to right in the third row, and vertical arrows from bottom to top in the third column.

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

scalar [*/m³]

1	1	1	1
1	1	1	1
1	1	2	1
1	1	1	1

Red arrows indicate advection: horizontal arrows from left to right in the third row, and vertical arrows from bottom to top in the third column.

scalar [*/kg]

		1	
		1.5	
1	1	1.5	

The time splitting problem

for simplicity: upstream advection, Courant number 0.5

y-x advection

x-y advection

density

1	1	1	1
1	1	1	1
1	→1	→1	1
1	1	1	1

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

density

		1	
		1.25	
1	1	0.75	

scalar [*/m³]

1	1	1	1
1	1	1	1
1	→1	→2	1
1	1	1	1

scalar [*/kg]

		1	
		1.5	
1	1	1.5	

scalar [*/m³]

		1	
		1.75	
1	1	1.25	

The time splitting problem

for simplicity: upstream advection, Courant number 0.5

y-x advection

x-y advection

density

1	1	1	1
1	1	1	1
1	→ 1	→ 1	1
1	1	1	1

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

density

		1	
		1.25	
1	1	0.75	

scalar [*/m³]

1	1	1	1
1	1	1	1
1	→ 1	→ 2	1
1	1	1	1

scalar [*/kg]

		1	
		1.5	
1	1	1.5	

scalar [*/kg]

		1	
		1.4	
1	1	1.67	

The time splitting problem

for simplicity: upstream advection, Courant number 0.5

y-x advection

x-y advection

density

1	1	1	1
1	1	1	1
1	→1	→1	1
1	1	1	1

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

scalar [*/m³]

1	1	1	1
1	1	1	1
1	→1	→2	1
1	1	1	1

scalar [*/kg]

		1	
		1.5	
1	1	1.5	

scalar [*/kg]

		1	
		1.4	
1	1	1.67	

mass gain
0.07

transport equation for substance with mass density ψ :

$$\frac{\partial \psi}{\partial t} = -\nabla \cdot (\psi \mathbf{v}) = -\sum_{i=1}^3 \frac{\partial}{\partial x_i} (\psi \dot{x}_i)$$

rewritten as

$$\frac{\partial \psi}{\partial t} = -\sum_{i=1}^3 \left[\frac{\partial}{\partial x_i} (\psi \dot{x}_i) - \psi \frac{\partial \dot{x}_i}{\partial x_i} \right] - \psi \nabla \cdot \mathbf{v}$$

Deformational correction algorithm

transport equation for substance with mass density ψ :

$$\frac{\partial \psi}{\partial t} = -\nabla \cdot (\psi \mathbf{v}) = -\sum_{i=1}^3 \frac{\partial}{\partial x_i} (\psi \dot{x}_i)$$

rewritten as

$$\frac{\partial \psi}{\partial t} = -\sum_{i=1}^3 \left[\frac{\partial}{\partial x_i} (\psi \dot{x}_i) - \psi \frac{\partial \dot{x}_i}{\partial x_i} \right] - \psi \nabla \cdot \mathbf{v}$$

calculated during 1d
advection steps

subtracted after 3d
advection step

Advection with deformational correction

for simplicity: upstream advection, Courant number 0.5

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

scalar [$**/\text{m}^3$]

1	1	1	1
1	1	1	1
1	1	2	1
1	1	1	1

Advection with deformational correction

for simplicity: upstream advection, Courant number 0.5

y-x advection

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

density

		1	
		1	
1	1	1	

scalar [$^{**}/m^3$]

1	1	1	1
1	1	1	1
1	1	2	1
1	1	1	1

scalar [$^{**}/m^3$]

		1	
		1.5	
1	1	1.5	

Advection with deformational correction

for simplicity: upstream advection, Courant number 0.5

y-x advection

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

scalar [*/m³]

1	1	1	1
1	1	1	1
1	1	2	1
1	1	1	1

scalar [*/kg]

		1	
		1.5	
1	1	1.5	

Advection with deformational correction

for simplicity: upstream advection, Courant number 0.5

y-x advection

x-y advection

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

Red arrows indicate advection: horizontal arrows from column 1 to 2 and 2 to 3; vertical arrows from row 2 to 1 and row 3 to 2.

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

density

		1	
		1	
1	1	1	

scalar [*/m³]

1	1	1	1
1	1	1	1
1	1	2	1
1	1	1	1

Red arrows indicate advection: horizontal arrows from column 1 to 2 and 2 to 3; vertical arrows from row 2 to 1 and row 3 to 2.

scalar [*/kg]

		1	
		1.5	
1	1	1.5	

scalar [*/m³]

		1	
		1.25	
1	1	1.75	

Advection with deformational correction

for simplicity: upstream advection, Courant number 0.5

y-x advection

x-y advection

density

1	1	1	1
1	1	1	1
1	→1	→1	1
1	1	1	1

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

scalar [*/m³]

1	1	1	1
1	1	1	1
1	→1	→2	1
1	1	1	1

scalar [*/kg]

		1	
		1.5	
1	1	1.5	

scalar [*/kg]

		1	
		1.25	
1	1	1.75	

- time splitting errors
 - both schemes: dependency on time splitting sequence
 - operational scheme: **only** consistent with density advection
- mass errors due to diagnostic density

→ Which time splitting algorithm is recommended?

→ tests with real case studies

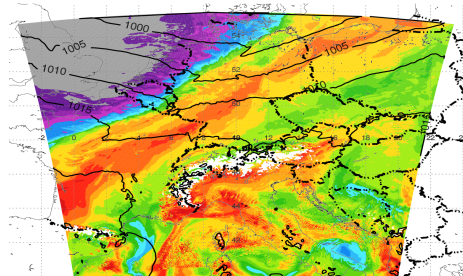
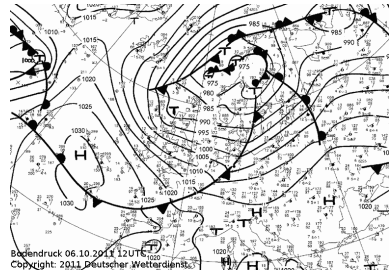
model set up

- fourth order Bott scheme
- no divergence damping
- different Strang splitting approaches:
 - operational approach xyz- and zy-advection alternating (Δt)
 - true Strang splitting zxyz advection ($\Delta t/2$)
 - double Strang splitting zyxy z yxyz ($\Delta t/4$)
- different resolutions (DE, EU)
- operational (ref) and deformational correction (dc) algorithm
- passive tracer

Weather Situation

requirements:

- strong deformational flow
 - alpine region
 - meteorological fronts
- example October 6, 2011

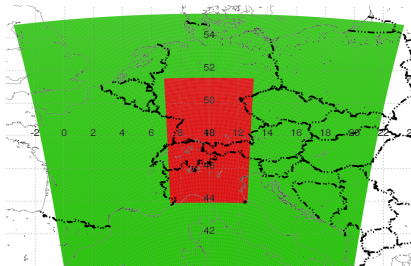


Pseudopotential temperature [°C] 850hPa, Sea level pressure [hPa]

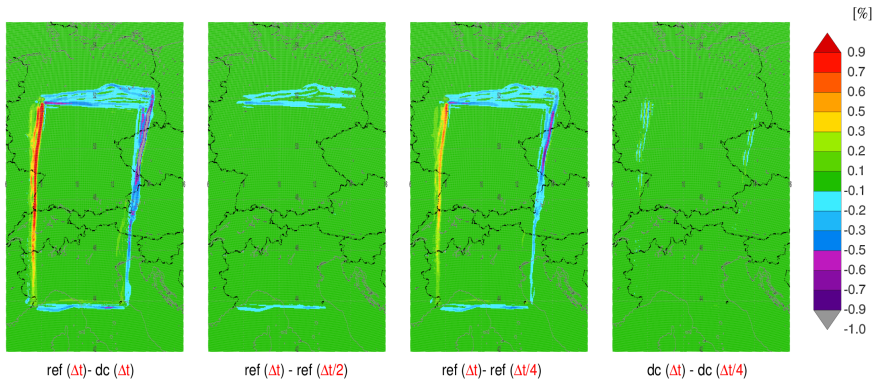
≤20.0 (Δ = 2.00) ≥50.0

Tracer initialization

- strong gradients
- box centered over alpine region
- pure advection

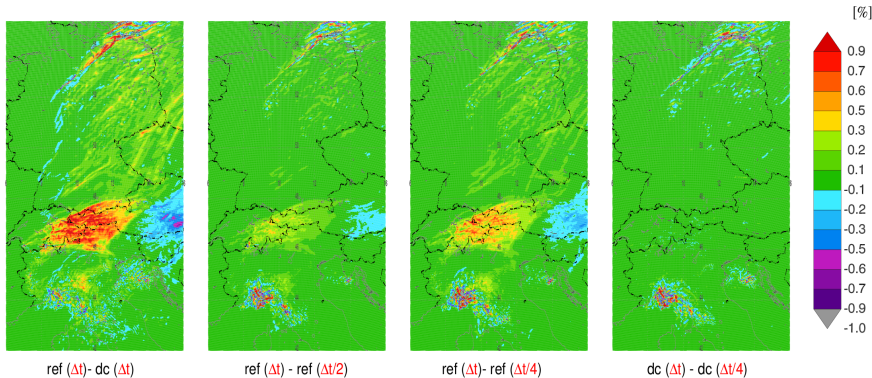


Tracer advection



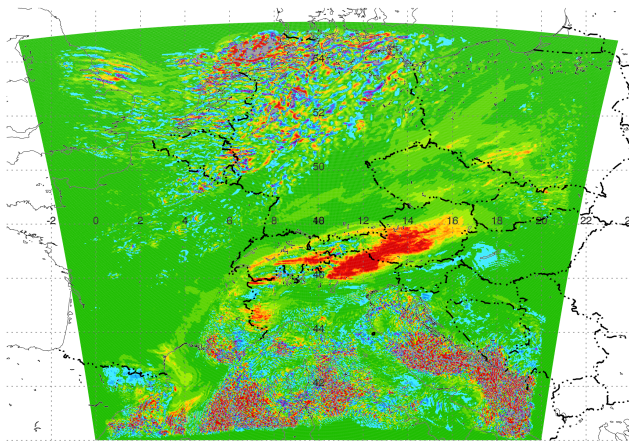
vertically integrated tracer mass difference (1h forecast)

Tracer advection

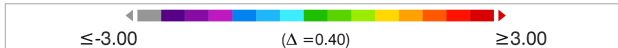


vertically integrated tracer mass difference (12h forecast)

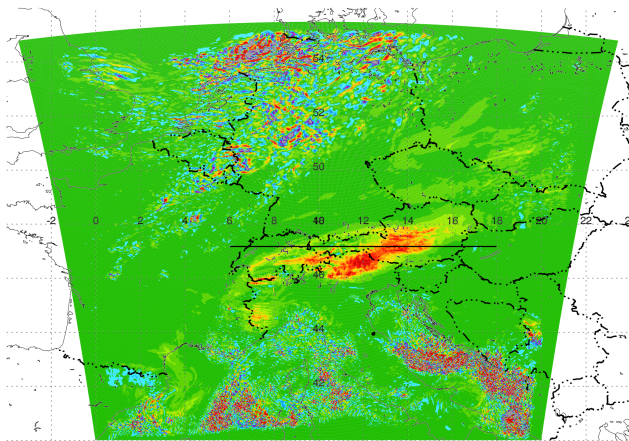
Specific humidity difference (12h forecast)



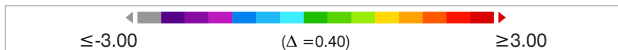
Specific humidity (integrated), ref - dc advection [%]



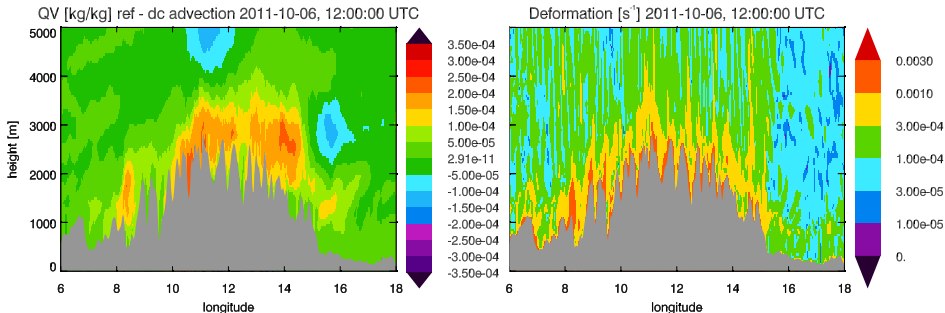
Specific humidity difference (12h forecast)



Specific humidity (integrated), ref - ref ($\Delta t/4$) advection [%]



Vertical cross section

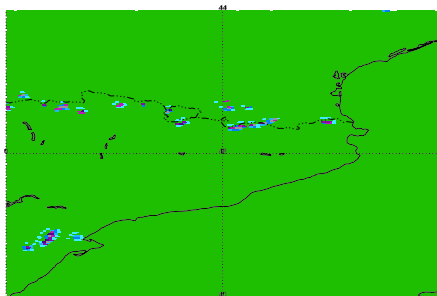


$$Def = \sqrt{\delta_{st}^2 + \delta_{sh}^2} \quad \text{with}$$

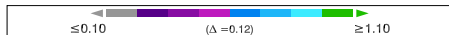
$$\delta_{st} = \frac{\partial u}{\partial x} - \frac{\partial v}{\partial y}$$

$$\delta_{sh} = \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y}$$

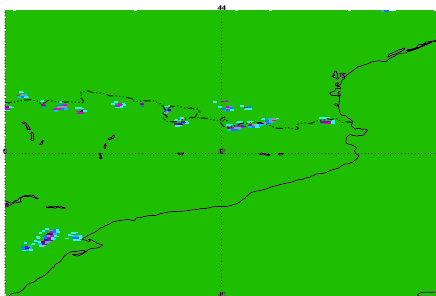
Mass implosions (05.01.12 00UTC +5min)



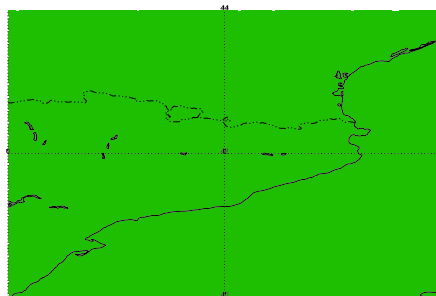
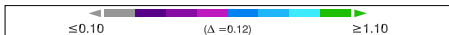
Tracer 10 lev ke (ref advection)



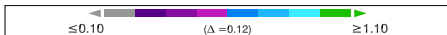
Mass implosions (05.01.12 00UTC +5min)



Tracer 10 lev ke (ref advection)



Tracer 10 lev ke (dc advection)

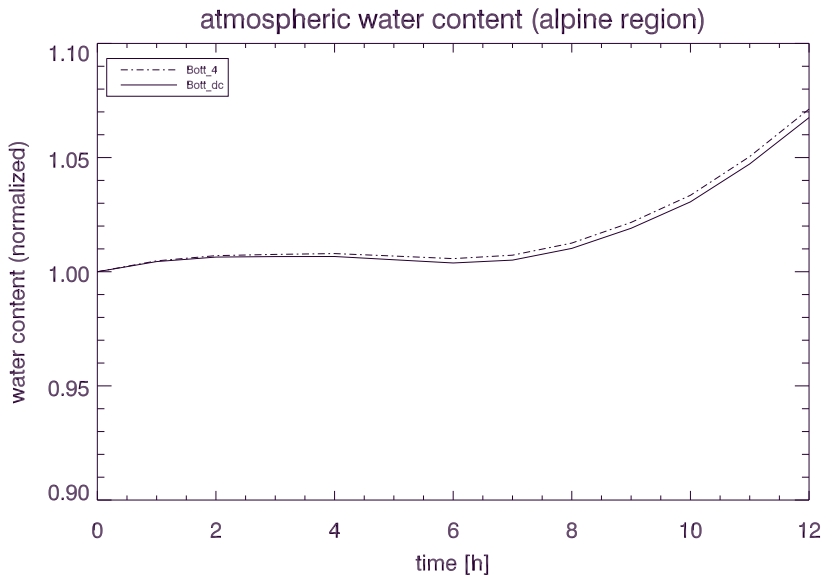


- Typical shortcomings of 1d flux-form advection schemes
 - results depend on time splitting approach
 - mass error due to diagnostic density
- Improvements with deformational correction
 - better representation of physical flow fields
 - hardly any dependency on time splitting approach
 - high accuracy without timestep reduction
 - improvement of mass balance
- Remaining problems
 - long term tests required to check improvement of model stability
 - time splitting errors are not completely corrected

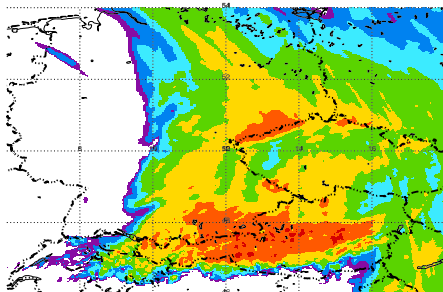


Thank you for your attention!

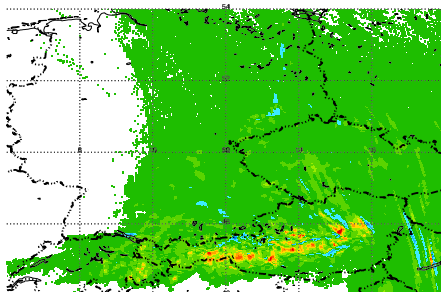
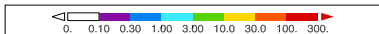
- Bott, A., Improving the time-splitting errors of one-dimensional advection schemes in multidimensional applications. Atmospheric Research, 97, pp619-631 (Sep. 2010)
- Schneider, W. and Bott, A ., On the time splitting errors of one-dimensional advection schemes in numerical weather prediction models (to be submitted)



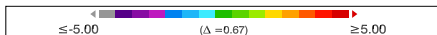
Effects on precipitation (orographic rain 05.01.2013)



total precipitation [l/m^2] 04.01.2013 12UTC + 36h



total precipitation (ref - dc advection) [l/m^2]



Advection with deformational correction

upstream advection, Courant number 0.5 (x-y advection)

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

scalar [*/kg]

1	1	1	1
1	1	1	1
1	1	2	1
1	1	1	1

Advection with deformational correction

upstream advection, Courant number 0.5 (x-y advection)

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

scalar [*/m³]

1	1	1	1
1	1	1	1
1	1	2	1
1	1	1	1

Advection with deformational correction

upstream advection, Courant number 0.5 (x-y advection)

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

scalar [*/m³]

1	1	1	1
1	1	1	1
1	1	2	1
1	1	1	1

density

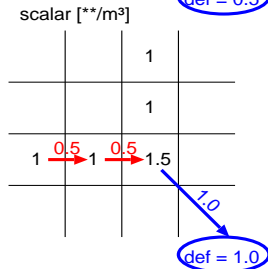
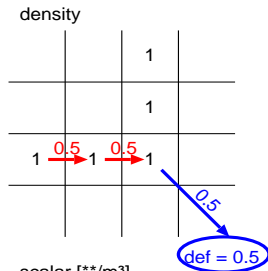
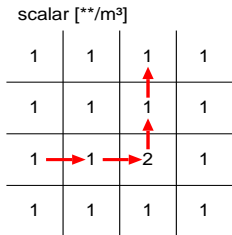
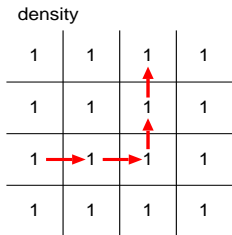
1	1	1	1
1	1	1	1
1	0.5	1	0.5
1	1	1	1

scalar [*/m³]

1	1	1	1
1	1	1	1
1	0.5	1	0.5
1	1	1	1

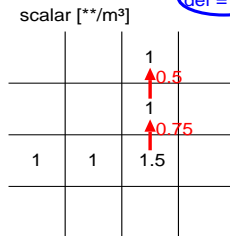
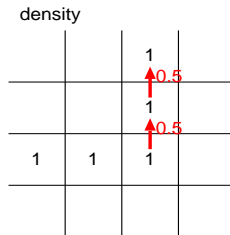
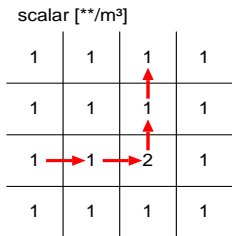
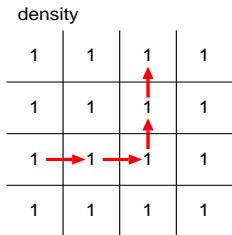
Advection with deformational correction

upstream advection, Courant number 0.5 (x-y advection)



Advection with deformational correction

upstream advection, Courant number 0.5 (x-y advection)

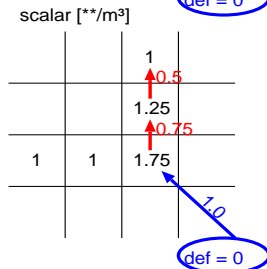
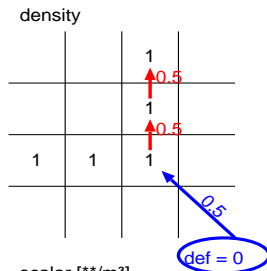
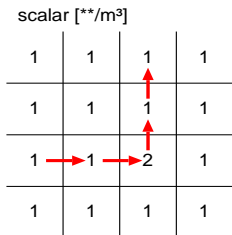
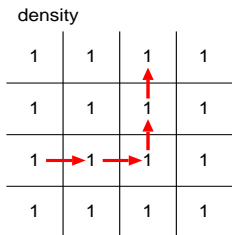


def = 0.5

def = 1.0

Advection with deformational correction

upstream advection, Courant number 0.5 (x-y advection)



Advection with deformational correction

upstream advection, Courant number 0.5 (x-y advection)

density

1	1	1	1
1	1	1	1
1	1	1	1
1	1	1	1

density

		1	
		1	
1	1	1	

scalar [*/m³]

1	1	1	1
1	1	1	1
1	1	2	1
1	1	1	1

scalar [*/kg]

		1	
		1.25	
1	1	1.75	

Idealized flow field tests

