

New features of the common turbulence parameterization for COSMO and ICON

Remaining Characteristics:

- ✓ represented in the **module TURBDIFF**: now common for COSMO and ICON
- ✓ **2-nd order turbulence closure at level 2.5** according MY (prognostic TKE-scheme)
- ✓ scale-separated through the **constraints of specific closure assumptions**
- ✓ applied also as the **core of surface-to-atmosphere transfer (SAT)** formulation

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Main supplements of the revised ICON-formulation:

technical

- In block-data structure
- Stronger modularization
- Including an universal VDiff SUB for ALL main- and half-level variables included in TURBDIFF
- Configurable by list of switches: including current COSMO-version

organization in COSMO

- Vertical diffusion optionally in “ICON-mode”:
 - called together with turbulence model
 - applied to mass-centered profiles

turbulence model

- Optional 3D-turbulence: 3D-wind-shear, application horizontal-diffusion coefficients
- One additional STIC term (due to separated SGS horizontal shear circulations) reformulated and active
- Different numerical treatment of vertical diffusion and circulation term in prognostic TKE-equation
- Less restrictive prevention of possible singularities

SAT model

- Complete moist physics applied to surface level: SGS fog-description possible
- Near-surface interpolation of vertical profiles in conserved variables
- Zero-concentration condition for q_i and q_c at the surface: deposition of droplets

empirical parameterizations

- Substituting badly tunable parameters by functions of the model variables

$tk(h,m)_{min}$, pat_len , a_hshr , rat_sea , $alfa0$, vel_min

The 3D-extension of TURBDIFF:

- Complete linear system of all 2-nd order equations needs to be solved **without BLA** in principal
- Simplification by an **analog extension of the SC-solution** (similar to Smagorinsky-type schemes):

$$\overline{\rho\phi_k''v_j''}^* = \begin{cases} \overline{\rho\phi_k''v_j''} \approx -\bar{\rho}K^H\partial_j\hat{\phi}_k & , \phi_k \text{ is a scalar} \\ \overline{\rho v_i''v_j''} - \delta_{ij}\bar{\rho} \cdot \left(\frac{q^2}{3} + K^M \frac{2}{3} \cancel{\nabla \cdot \hat{\mathbf{v}}} \right) \approx -\bar{\rho}K^M(\partial_i\hat{v}_j + \partial_j\hat{v}_i) & , \phi_k = v_i \quad \text{trace-less stress tensor} \end{cases}$$

$$Q_{3DS}^{TKE} = -\sum_{i,j} \overline{\rho v_i''v_j''} \partial_i\hat{v}_j \approx \bar{\rho}K^M \left[\underbrace{\frac{1}{2} \sum_{i \neq j} (\partial_i\hat{v}_j + \partial_j\hat{v}_i)^2 + 2 \sum_i (\partial_i\hat{v}_i)^2 - \frac{2}{3} (\cancel{\nabla \cdot \hat{\mathbf{v}}})^2}_{F^M \leftrightarrow F_{3D}^M} \right] - \bar{\rho} \frac{q^2}{3} \cancel{\nabla \cdot \hat{\mathbf{v}}}$$

$F^M \leftrightarrow F_{3D}^M$ complete direct 3D shear by the GS flow

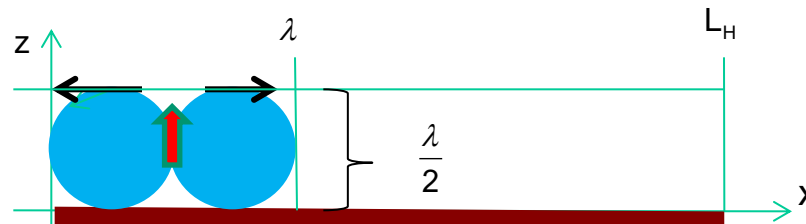
$$K^{M,H} = qS^{M,H}\ell \quad \text{turbulent isotropic diffusion coefficients with stability functions similar to HBA but } F^M \leftrightarrow F_{3D}^M$$

- Turbulent length scale restriction by horizontal grid scale L_H :

scale adaptivity

$$\ell = \kappa \cdot \text{MAX} \left\{ \frac{z \cdot z_m}{z + z_m}, \frac{L_H}{2} \right\}$$

z_m : maximal asymptotic turbulent distance 'tur_len'

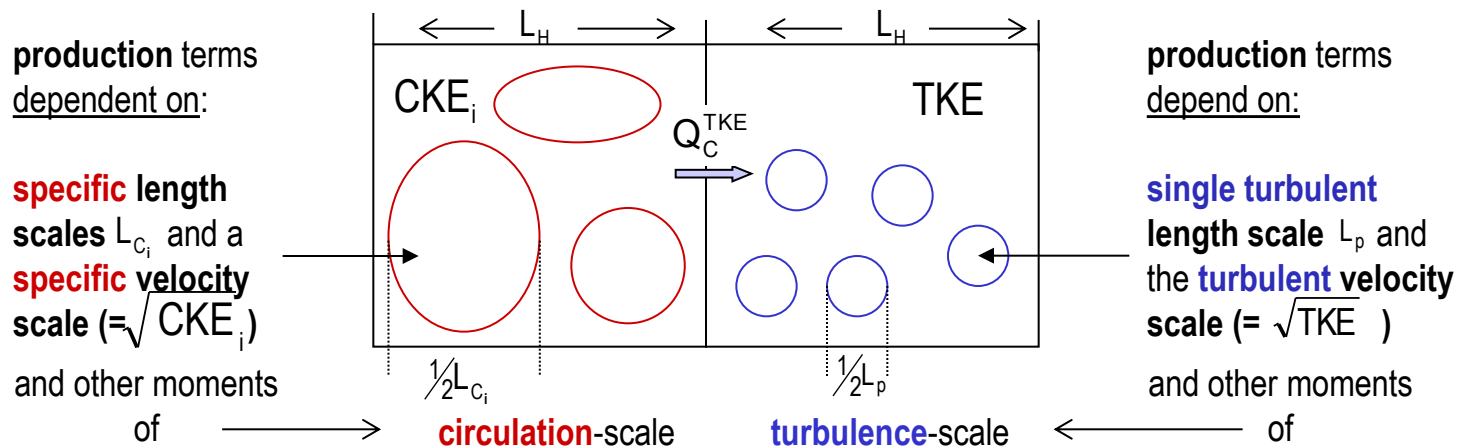


- Additional terms in budgets of ϕ_k by **convergence of additional horizontal fluxes** and (a not yet implemented) **kinematic pressure correction**

The coarse resolution extension of TURBDIFF:

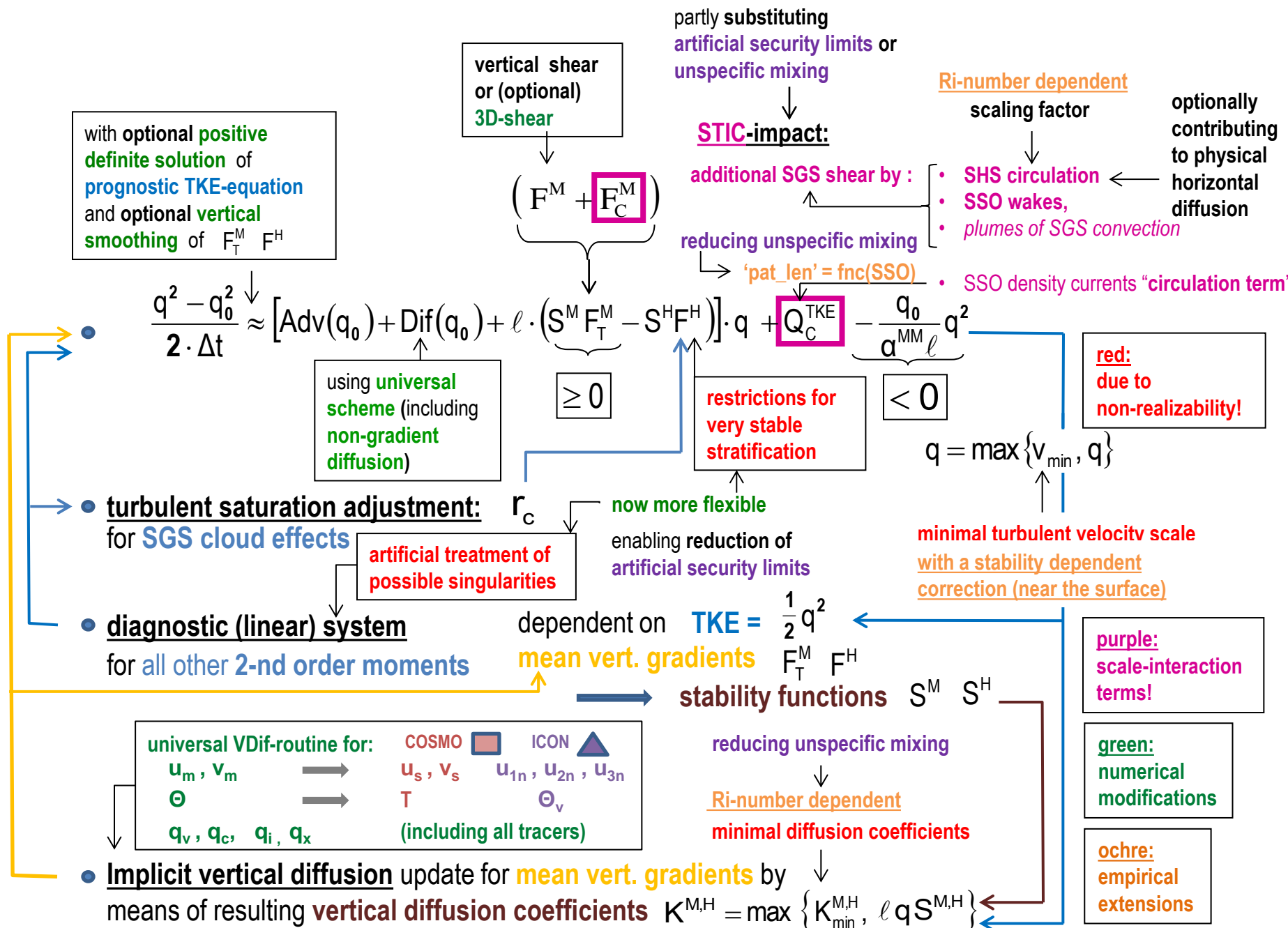
→ **STIC**: **S**eparated **T**urbulence **I**nteracting with non-turbulent **C**irculations

- Application of turbulence approximations only to small SGS scales $\leq L = \min\{L_p, L_H\}$
 - separation of the sub grid scale flow in different classes with specific closure assumptions
 - by application of associated filter scales
- turbulent budgets with additional production terms due to shear terms with respect to the separated sub grid scale circulation flow of
 - wake vortices by SSO (sub grid scale orography) blocking or gravity wave breaking [operational in COSMO and ICON]
 - large separated horizontal shear vortices [operational in ICON]
 - surface induced density flow patterns [operational in COSMO and ICON]
 - shallow and deep convection patterns [not yet operational active]



Q_C^{TKE} is the **scale interaction term** shifting SKE from the circulation part of the spectrum (CKE) to the turbulent part (TKE) by virtue of shear generated by the circulation flow patterns.

Practical solution within the time loop:



The roughness layer extension of TURBDIFF:

→ **S**urface-to-**A**tmosphere **T**ransfer (**SAT**) expressed by turbulence scheme

- Vertical integration of **effective flux densities** within a **Constant Flux Layer (CFL)** close to the surface
 - application of the **turbulence scheme** at the **lower model boundary**
 - considering **surface enlargement** by **land use**
 - using **proper vertical interpolation function** of **turbulent velocity scale**

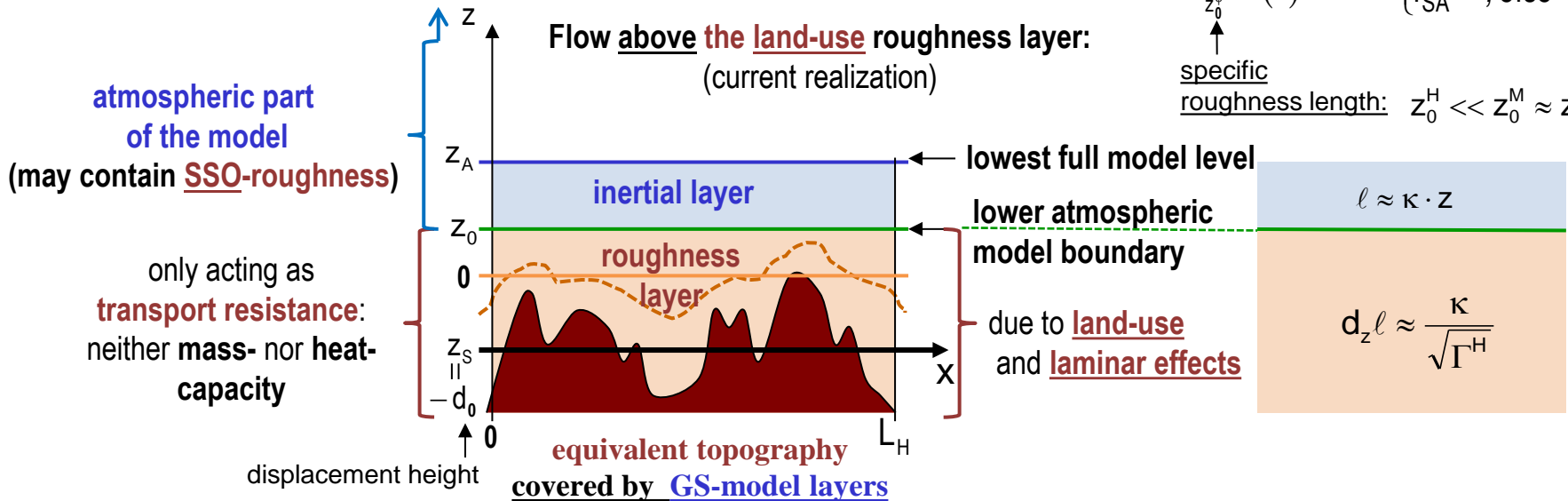
$$\tilde{f}^\phi(z) \approx -\Gamma^\phi \cdot \left(k^\phi + qS^\phi \ell \right) \cdot \partial_z \hat{\phi} =: -\Gamma^\phi u^\phi(z) \cdot \ell(z) \cdot \partial_z \hat{\phi} = -\frac{\hat{\phi}(z_A) - \hat{\phi}(z_S)}{r_{SA}^\phi}$$

squared specific surface area index molecular diffusion coefficient turbulent length scale effective velocity scale total transfer resistance

$$r_{SA}^\phi = \int_{z_S}^{z_0} \frac{dz}{\Gamma^\phi u^\phi(z) \cdot \ell(z)} + \int_{z_0}^{z_A} \frac{dz}{v^\phi(z) \cdot \kappa Z}$$

$$=: \int_{z_0^\phi}^{z_A} \frac{dz}{v^\phi(z) \cdot \kappa Z} = \begin{cases} r_{SA}^M & , \phi \in \{v_1, v_2\} \\ r_{SA}^H & , \text{else} \end{cases}$$

specific roughness length: $z_0^H \ll z_0^M \approx z_0$



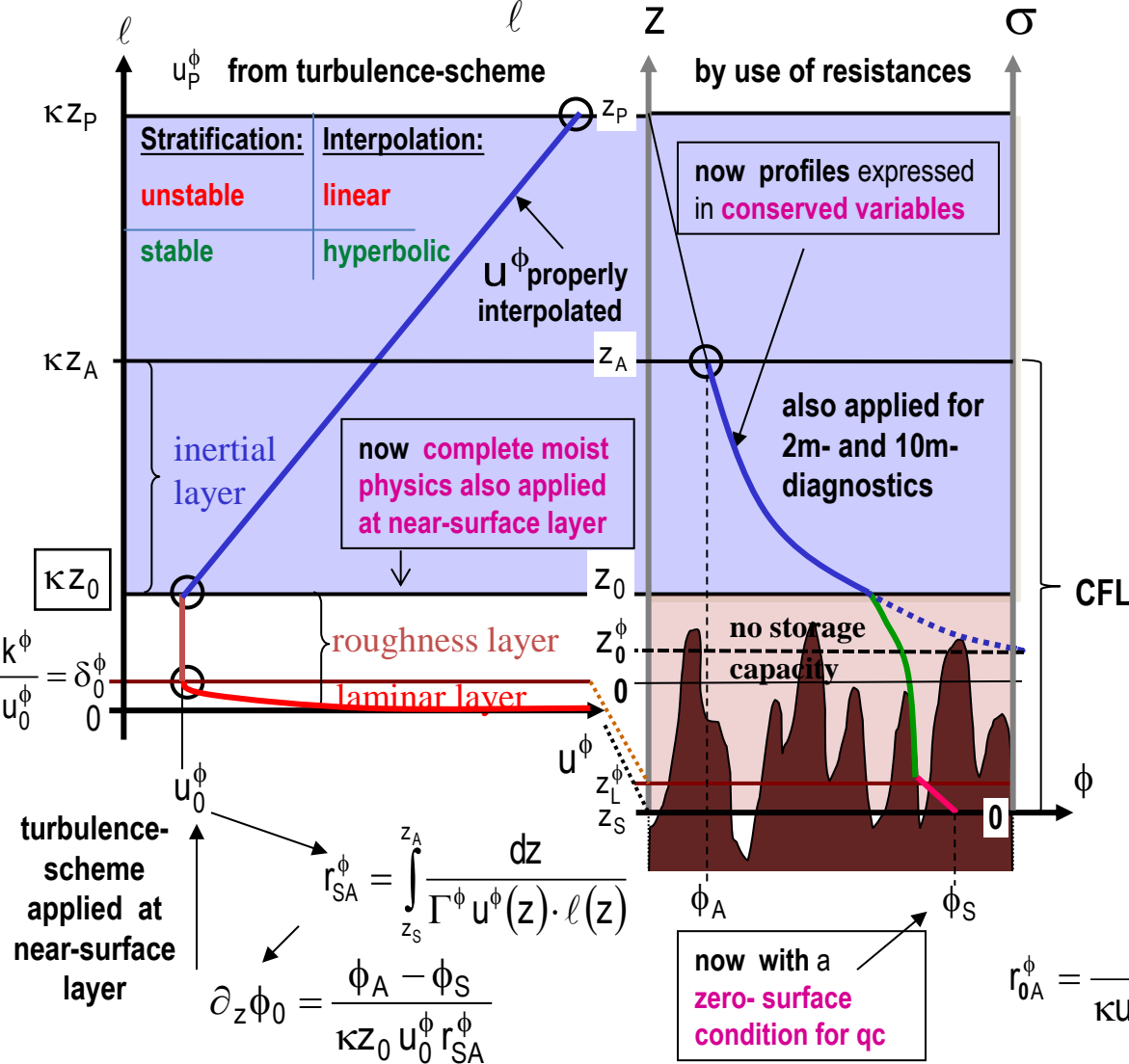
Main differences in surface-layer part:

expected to be necessary for **strong stable stratification** and a **homogeneous surface**

Effective velocity- scale

$$\text{profile } u^\phi := \frac{K^\phi + k^\phi}{\ell}$$

Mean variable profile



➤ Roughness-layer resistance for scalars:

$$r_{s0}^H = \frac{1}{\kappa U_0^H \cdot S_{Al_0}} \cdot \left(\lambda^H + \ln \frac{\kappa z_0 U_0^H}{k^H} \right)$$

effective value of $\sqrt{\Gamma^H}$

now with a laminar scaling parameter dependent on $\partial_z \theta_0$ over see surfaces

➤ Inertial-layer resistance:

stability-parameter of vertical profile-function

$$\gamma_s^\phi := \frac{z_0}{z_p - z_0} \left[\frac{u_p^\phi}{u_0^\phi} - 1 \right] = 1 - \frac{u_*}{u_0^\phi} \frac{S_0^\phi}{S_0^M}$$

now optionally without using the upper interpolation node u_p^ϕ

now optionally with the additional **stable branch**

$$r_{0A}^\phi = \frac{1}{\kappa U_0^\phi \cdot (1 - \gamma_s^\phi)} \cdot \begin{cases} \ln \left(\frac{z_A}{z_0} \right) - \gamma_s^\phi \frac{z_A - z_0}{z_0}, & \gamma_s^\phi < 0 \\ \ln \left[\frac{z_A}{z_0 + \gamma_s^\phi \cdot (z_A - z_0)} \right], & \gamma_s^\phi \geq 0 \end{cases}$$

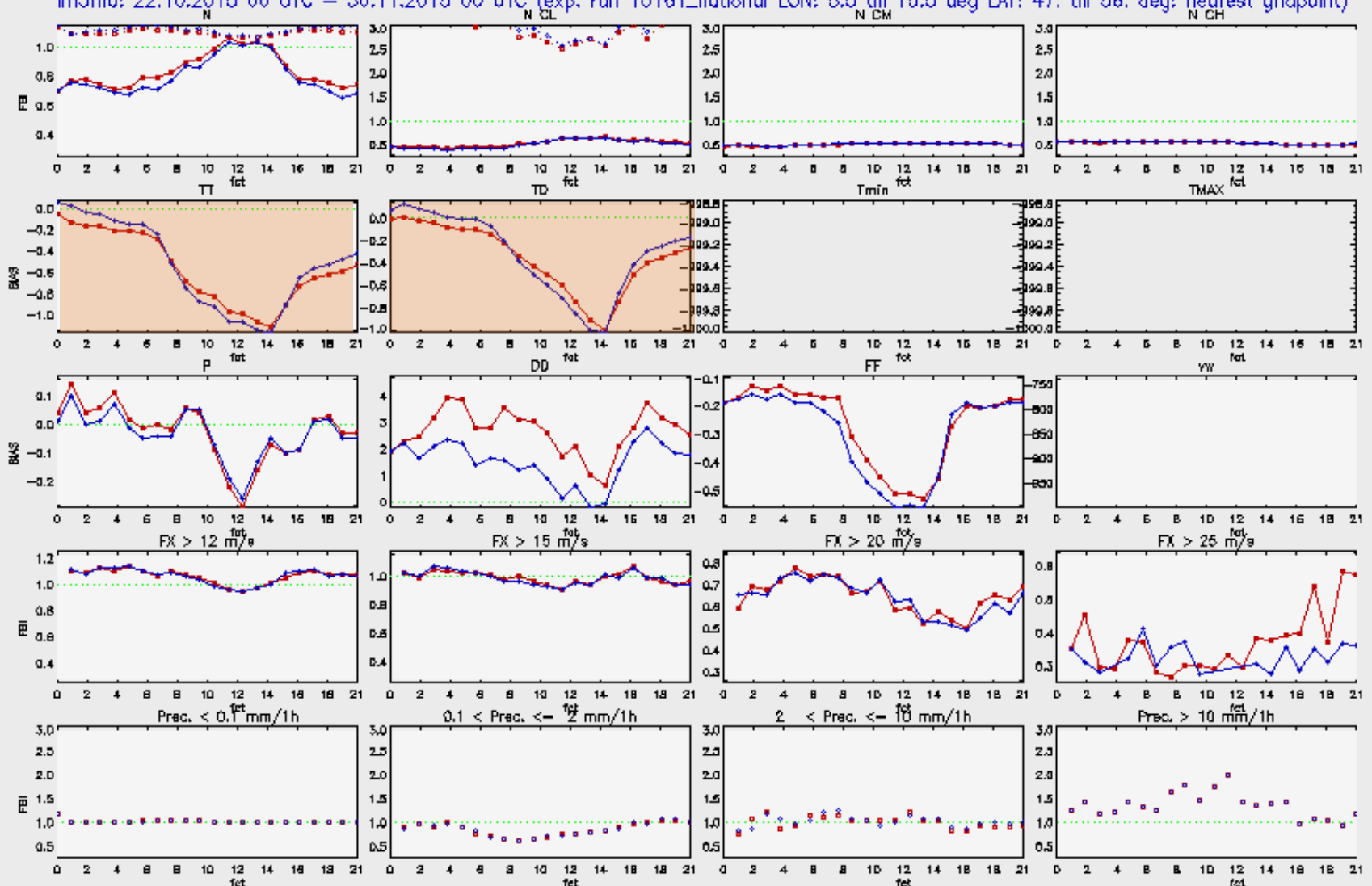
stable

unstable

operational <-> new TURBDIFF (ICON-settings; ICON-like V-Diff):

BIAS for late Autumn 2015:

LM3MO: 22.10.2015 00 UTC – 30.11.2015 00 UTC (exp. run 10127_national: ICON Antrieb neues Turbulenschema mit ICON settings vertikale Diff
 lm3mo: 22.10.2015 00 UTC – 30.11.2015 00 UTC (exp. run 10161_national LON: 5.5 till 15.5 deg LAT: 47. till 56. deg; nearest gridpoint)



Results of verification of forecasts for local weather elements at surface stations

FBI for cloud covers gusts and precipitation, BIAS for other elements

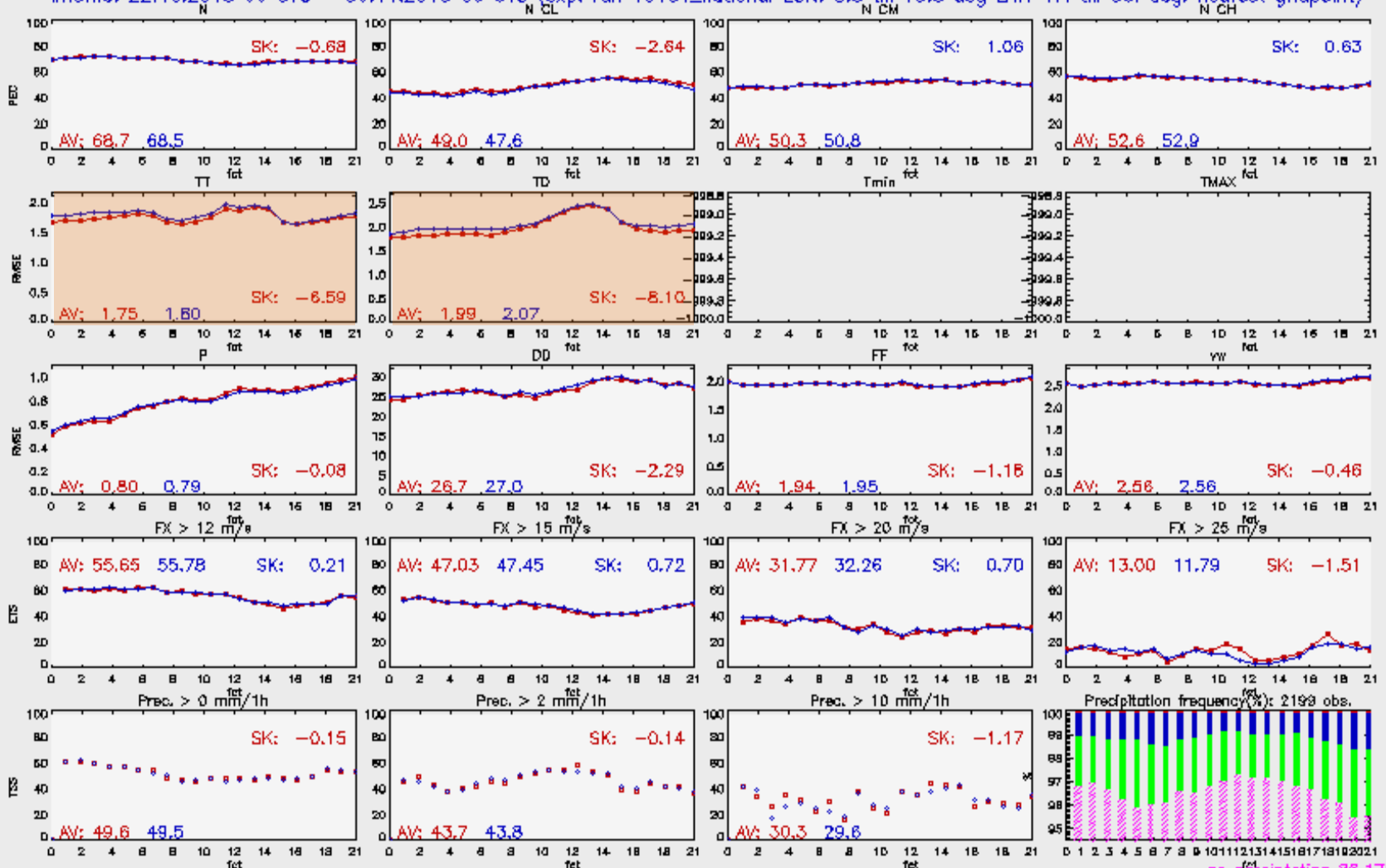
All stations

Plottime: 15.01.2016 18:14:07 MEZ

operational <-> new TURBDIFF (ICON-settings; ICON-like V-Diff):

RMSE for Autumn 2015:

LM3MO: 22.10.2015 00 UTC – 30.11.2015 00 UTC (exp. run 10127_national: ICON Antrieb neues Turbulenschema mit ICON settings vertikale Diff
 lm3mo: 22.10.2015 00 UTC – 30.11.2015 00 UTC (exp. run 10161_national LON: 5.5 till 15.5 deg LAT: 47. till 56. deg; nearest gridpoint)



Results of verification of forecasts for local weather elements at surface stations

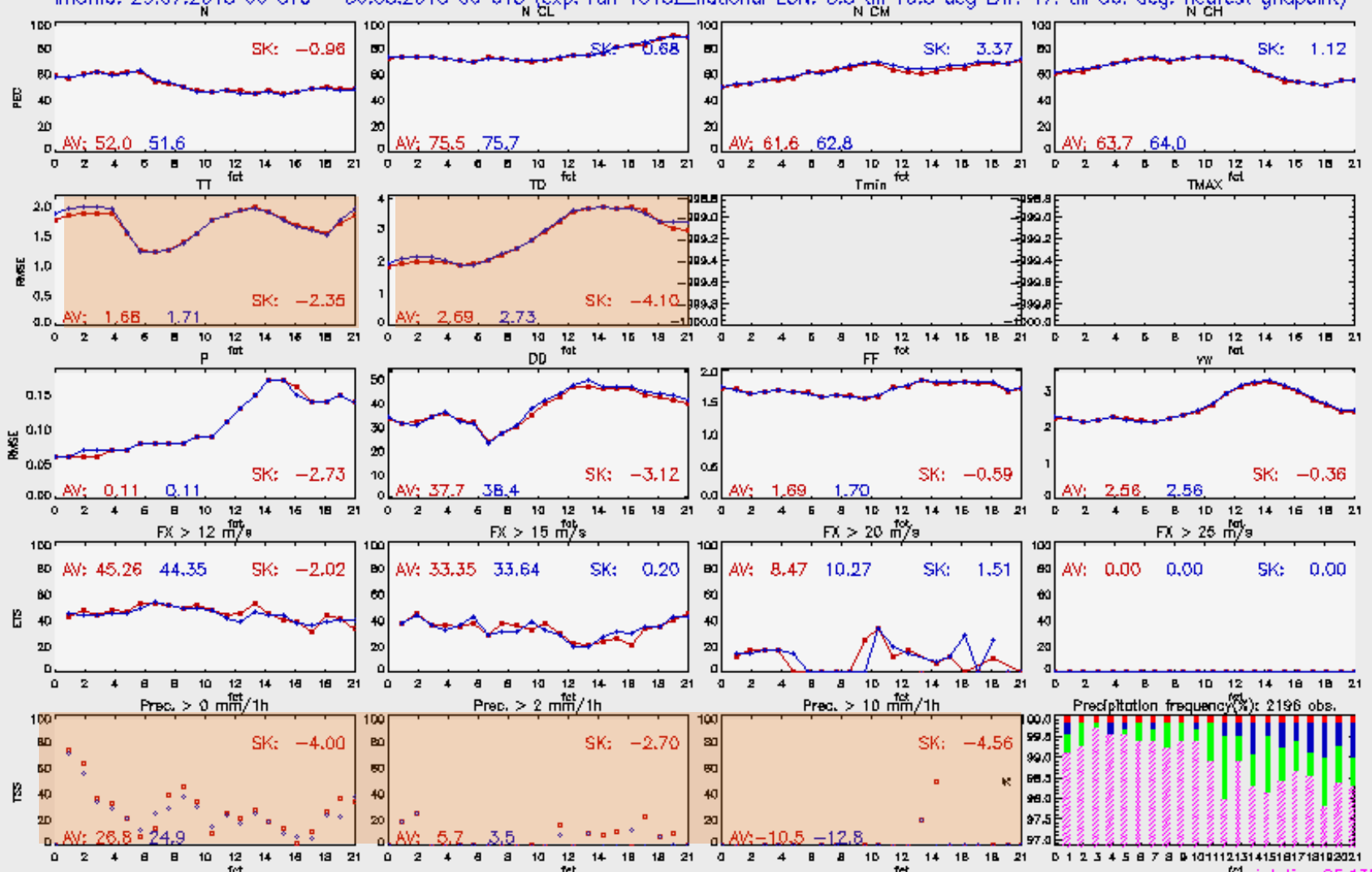
TSS for precipitation, ETS for gusts, percent correct for cloud covers, RMSE for other elements

no precipitation 86.17%
 0.1–2 mm: 10.43%
 2–10 mm: 2.28%
 > 10 mm: 1.12%

operational <-> new TURBDIFF (ICON-settings; ICON-like V-Diff):

RMSE for August 2015:

LM3MO: 29.07.2015 00 UTC – 30.08.2015 00 UTC (exp. run 10188_national: ICON Antrieb neuer Turb. Schema mit ICON Settings vert. diff. von
 lm3mo: 29.07.2015 00 UTC – 30.08.2015 00 UTC (exp. run 10152_national LON: 5.5 till 15.5 deg LAT: 47. till 56. deg; nearest gridpoint)



Results of verification of forecasts for local weather elements at surface stations

TSS for precipitation, ETS for gusts, percent correct for cloud covers, RMSE for other elements

Plattime: 28.01.2018 15:12:35 MEZ

All stations

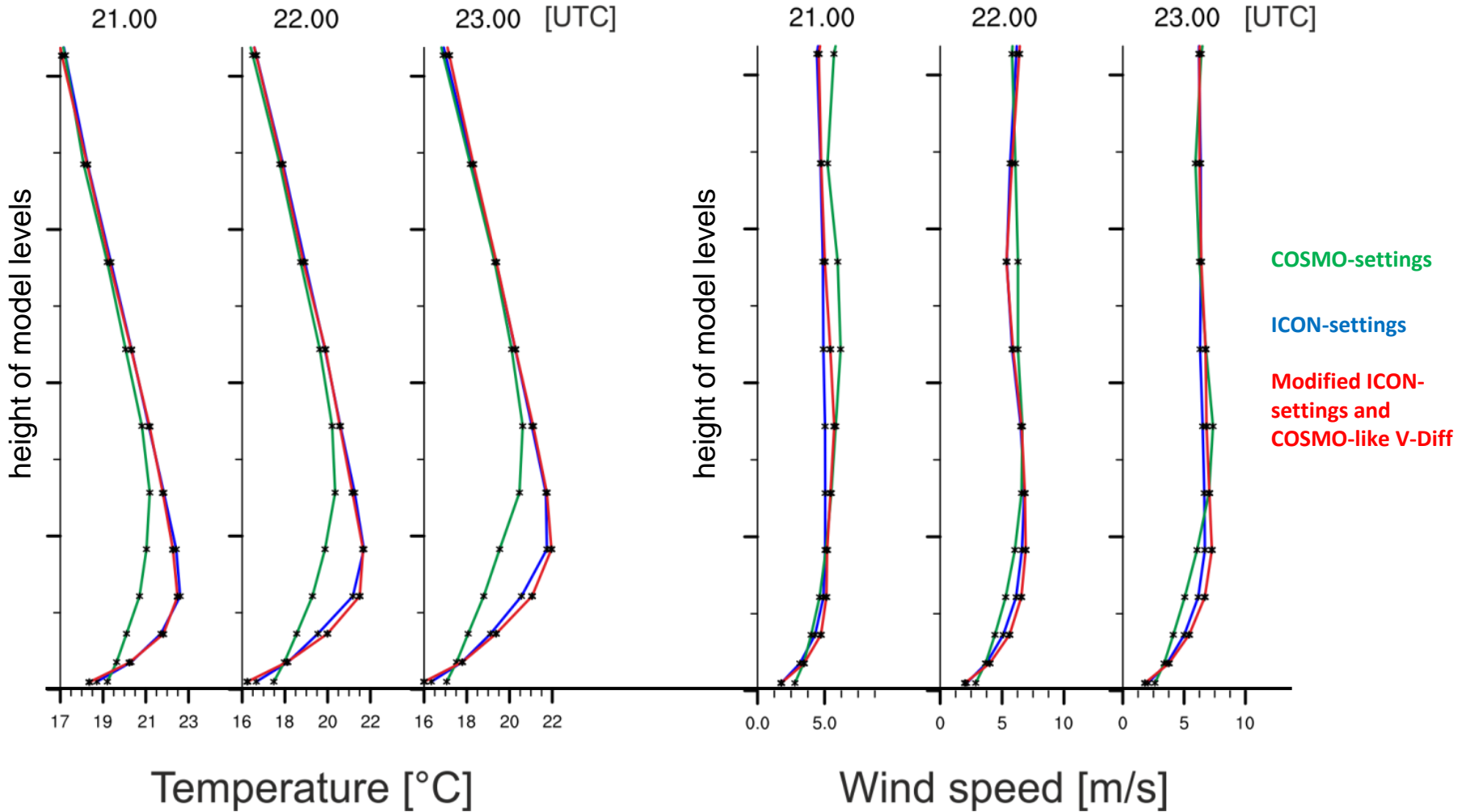
Precipitation frequency (%): 2196 obs.
 no precipitation 95.13%
 0.1–2 mm: 3.89%
 3–10 mm: 0.88%
 > 10 mm: 0.32%

Vertical profiles at night hours (for different TURBDIFF-configurations):



Deutscher Wetterdienst
Wetter und Klima aus einer Hand

Falkenberg, July 03, 2014



EWeLiNE



Deutscher Wetterdienst
Wetter und Klima aus einer Hand



Tennet
Taking power further



Fraunhofer
IWES

provided by Andrea Steiner (DWD)

A conclusion:

- Too much **unspecific mixing** and **security measures** had been active before



Double strategy:

➤ Improving physical parameterizations:

- More specific and complete **scale interaction terms**

dependent on **model parameters**

➤ Optimization of parameter values:

- Reduction of **unspecific background mixing** to the necessary minimum
- Improving **empirical/statistical parameterizations**:
 - Substituting **non-tunable parameters** by **functions of the model state**

dependent on **regression parameters**

Diagnostics of the special SAT-approach in TURBDIFF:

- Our generalizations are due to a direct application of the turbulence scheme and its generalizations:

explicit description of the roughness-and laminar-layer resistance



substituting a **specific roughness length for scalars** being an **unspecific parameter**

scale interaction terms



additional shear



reduced Ri-numbers for **stable stratification**



physically based “tail” for **stable stratification** mainly at heterogeneous surfaces

- The **desired additional mixing** for **stable stratification** is rather too intensive than too weak!
 - a) What is the effect of **remaining unspecific turbulence enhancing measures**?
 - b) Is the scheme in accordance to a MOS solution, which is valid for a homogeneous surface?

Definitions of boundary layer properties:

$$\underline{r^\phi} := \Gamma^\phi \cdot \left(\frac{k^\phi}{v^\phi \ell} + \mathbf{1} \right) \quad \text{correction factor for roughness and laminar effects}$$

$$\boxed{F_T^M := F^M + F_C^M} \quad \text{generalized squared wind shear frequency} \\ \text{(including contribution by non turbulent circulations)}$$

$$G_T^M := \frac{\ell^2}{q^2} \cdot F_T^M \geq \mathbf{0}$$

$$F^H := \frac{g}{\hat{\theta}_v} \partial_z \hat{\Theta}_v \quad \text{generalized square for Brunt-Väisälä-frequency} \\ \text{(including contribution by sub grid scale condensation)}$$

$$G_T^H := \frac{\ell^2}{q^2} \cdot F^H$$

$$R_i := \frac{F^H}{r^M F^M} \quad \text{Richardson number}$$

$$R_f := \frac{S^H}{S^M} R_i \quad \text{Richardson flux number}$$

$$u_*^2 := \underline{r^M} v^M \sqrt{F_T^M} \quad \text{generalized square friction velocity}$$

$$u_* \theta_* := -\frac{\hat{\theta}_v}{g} \underline{r^H} v^H F^H \quad \text{generalized buoyancy heat flux}$$

$$L_{MO} := -\frac{u_*^2 \hat{\theta}_v}{g \theta_*} \quad \text{Monin-Obukhov stability length scale}$$

vertically constant
in transfer layer

$$\boxed{\psi^\phi := \frac{v^\phi}{u_*}} \quad \text{vertical profile functions}$$

MY-like SC-solution with a quasi-diagnostic TKE-equation:

$$\gamma := 1 + \alpha^{MM} \frac{\ell}{q} \frac{D_t \left(\frac{1}{2} \bar{\rho} q^2 \right)}{\bar{\rho} q^2} = \alpha^{MM} \cdot (\underline{r}^M S^M G_T^M - S^H G^H) \quad \chi := \frac{R_f}{1 - R_f}$$



$$\alpha^{MM} \underline{r}^M S^M G_T^M = \gamma \cdot (1 + \chi)$$

$$S^H + \left[\gamma \frac{\alpha^H}{\alpha^{MM}} \left(\underline{3r}^H \alpha^{HH} + 18\alpha^M \right) \right] \cdot \chi = \alpha^H \left[(1 - 3c^H) - 6\gamma \frac{\alpha^M}{\alpha^{MM}} \right] =: b =: S_0^H$$

$$S^M + \left[\underbrace{\gamma \frac{\alpha^M}{\alpha^{MM}} \left(\underline{9r}^H \alpha^{HH} + 18\alpha^M \right)}_{=:c} + \underbrace{\gamma \frac{\alpha^M}{\alpha^{MM}} \left(\underline{9r}^M \alpha^H \right)}_{=:e} \frac{S^M}{S^H} \right] \cdot \chi = \alpha^M \left[(1 - 3c^M) - 6\gamma \frac{\alpha^M}{\alpha^{MM}} \right] =: d =: S_0^M$$

$a = 2.09$, $b = 0.49$, $c = 1.29$, $e = 0.37$, $d = 0.39$

$$\alpha := \frac{(a + b - e) \cdot R_i + d}{d + c} \quad \beta := \frac{b}{d + c} R_i$$

critical Ri-number

$$R_i < R_i^c := \frac{da - bc}{e \cdot (a + b)} > 0$$

$$\xrightarrow{\hspace{2cm}} R_f = \frac{\alpha}{2} - \sqrt{\frac{\alpha^2}{4} - \beta} \xrightarrow{\hspace{2cm}}$$

$$S^H = b - a\chi$$

$$S^M = \frac{(d - c\chi) \cdot (b - a\chi)}{b - (a - e)\chi}$$

The revised vertical profile function in accordance with turbulence model:

$$\longrightarrow R_f \cdot \frac{r^H}{r^M} \frac{L_{MO}}{\ell} = \psi^M = \left[\frac{\alpha^{MM}}{r^M} S^{M3} \cdot (1 - R_f) \right]^{1/4}$$

S^M
 S^H are function of R_f

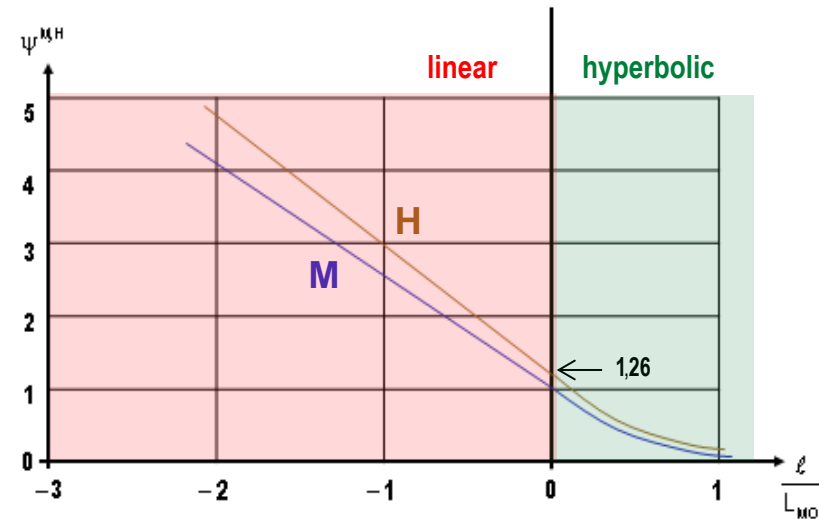
$$\psi^H = \frac{S^H}{S^M} \psi^M$$



$$\psi_0^M = 1$$

constant dependent on
 r^M and r^H

$$\frac{v^\phi}{u_*} = \psi^\phi \approx \psi_0^\phi \cdot \begin{cases} 1 + \alpha^\phi \frac{\ell}{L_{MO}} & \text{unstable} \\ \left(1 + \alpha^\phi \frac{\ell}{L_{MO}} \right)^{-1} & \text{stable} \end{cases}$$



- In accordance with **MOS-solution** as well as **measurements** (Businger-profiles) above **homogeneous surfaces**, where $F_T^M = F^M$

- Notice:

- **Parameters of MY-scheme** have been evaluated in order to match with these measured profile functions!
- **Artificial “long tail”** substituted by **decreasing** $\left| \frac{\ell}{L_{MO}} \right|$ due to **additional TKE-sources**

- Can this finding be confirmed by **component tests** for **inertial layer resistance**?



next talk